

CLAIM AMENDMENTS

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32. (CURRENTLY AMENDED) A drive circuit for a micromechanical resonator, which has at least one pulse modulator for conversion of a complex input signal to a pulsed signal, and which has:

- a subtraction stage which produces a control error signal from the difference between the complex input signal and a feedback signal;
- a signal ~~single~~ conversion stage, which converts the control error signal to a control signal;
- a first multiplication stage, which multiplies the control signal by a complex mixing signal oscillating at the frequency  $\omega_0$ , and thus produces at least one of a real part and an imaginary part of a control signal which has been up-mixed by  $\omega_0$ ,
- a quantization stage, which quantizes at least one of the real part and imaginary part of the control signal which has been up-mixed by  $\omega_0$  and thus produces the pulsed signal, with the pulsed signal which is produced by the at least one pulse modulator being used for electrostatic oscillation stimulation of a resonator, and with the pulse modulator being operated at a sampling frequency  $\omega_A$  which is 2 to 1000 times higher than the mixing frequency  $\omega_0$ ,
- a feedback unit, which uses the pulsed signal to produce the feedback signal for the subtraction stage.

- said first multiplication stage having a first multiplier for the in-phase signal path and a second multiplier for the quadrature signal path, with the first multiplier multiplying the real part of the control signal by the real part of the complex mixing signal oscillating at the frequency  $\omega_0$ , and thus producing a first result signal, and with the second multiplier multiplying the imaginary part of the control signal by the imaginary part of the complex mixing signal oscillating at the frequency  $\omega_0$ , and thus producing a second result signal; and
- the pulse modulator has an adder which adds the first result signal from the first multiplier and the second result signal from the second multiplier to form a sum signal in order to determine the real part of the up-mixed control signal.

33. (PREVIOUSLY PRESENTED) The drive circuit as claimed in claim 32, characterized in that the mixing frequency  $\omega_0$  of the pulse modulator corresponds to one resonant frequency of the resonator.

34. (PREVIOUSLY PRESENTED) The drive circuit as claimed in claim 32, characterized in that the pulse modulator has an in-phase signal path for processing of the real part of the input signal, as well as a quadrature signal path for processing of the imaginary part of the input signal.

35. (PREVIOUSLY PRESENTED) The drive circuit as claimed in claim 32, characterized in that the control error signal, the control signal and the feedback signal are each complex signals, which each have a real signal component as well as an imaginary signal component.

36. (PREVIOUSLY PRESENTED) The drive circuit as claimed in claim 32, characterized in that the signal conversion stage has an integrator stage which integrates the control error signal and produces an integrated signal as the control signal.

37. (PREVIOUSLY PRESENTED) The drive circuit as claimed in claim 36, characterized in that the integrator stage has a first integrator for the in-phase signal path and a second integrator for the quadrature signal path, with the first integrator integrating the real part of the control error signal, and with the second integrator integrating the imaginary part of the control error signal.

38. (PREVIOUSLY PRESENTED) The drive circuit as claimed in claim 32, characterized in that the signal conversion stage has an amplifier stage.

39. (CANCELED) The drive circuit as claimed in claim 32, characterized in that the first multiplication stage has a first multiplier for the in-phase signal path and a second multiplier for the quadrature signal path, with the first multiplier multiplying the real part of the control signal by the real part of the complex mixing signal oscillating at the frequency  $\omega_0$ , and thus producing a first result signal, and with the second multiplier multiplying the imaginary part of the control signal by the imaginary part of the complex mixing signal oscillating at the frequency  $\omega_0$ , and thus producing a second result signal.

40. (CANCELED) The drive circuit as claimed in claim 39, characterized in that the pulse modulator has an adder which adds the first result signal from the first multiplier and the second result signal from the second multiplier to form a sum signal in order to determine the real part of the up-mixed control signal.

41. (CURRENTLY AMENDED) The drive circuit as claimed in claim 32 ~~40~~, characterized in that the quantization stage quantizes the sum signal produced by the adder.

42. (PREVIOUSLY PRESENTED) The drive circuit as claimed in claim 32, characterized in that a noise level is added to the input signal to the quantization stage.

43. (PREVIOUSLY PRESENTED) The drive circuit as claimed in claim 32, characterized in that the quantization stage carries out binary quantization or ternary quantization of its respective input signal.



44. (PREVIOUSLY PRESENTED) The drive circuit as claimed in claim 32, characterized in that the feedback unit has a second multiplication stage, which multiplies the pulsed signal by a complex-conjugate mixing signal oscillating at the frequency  $\omega_0$ , and thus produces the feedback signal down-mixed by  $\omega_0$ , for the subtractor.

45. (PREVIOUSLY PRESENTED) The drive circuit as claimed in claim 44, characterized in that the second multiplication stage has a third multiplier for production of the real part of the feedback signal and has a fourth multiplier for production of the imaginary part of the feedback signal, with the third multiplier multiplying the pulsed signal by the real part of the complex-conjugate mixing signal oscillating at the frequency  $\omega_0$ , and with the fourth multiplier multiplying the pulsed signal by the imaginary part of the complex-conjugate mixing signal at the frequency  $\omega_0$ .

46. (PREVIOUSLY PRESENTED) The drive circuit as claimed in claim 32, characterized in that the pulse modulator is implemented with the aid of a digital signal processor.

47. (CANCELED) A frequency generator for synthesis of a pulsed signal at a predetermined frequency and with a predetermined phase, which has at least one pulse modulator for conversion of a complex input signal to a pulsed signal and which has:

- a subtraction stage which produces a control error signal from the difference between the complex input signal and a feedback signal,
- a single conversion stage, which converts the control error signal to a control signal;
- a first multiplication stage, which multiplies the control signal by a complex mixing signal oscillating at the frequency  $\omega_0$ , and thus produces at least one of a real part and an imaginary part of a control signal which has been up-mixed by  $\omega_0$ , with the pulse modulator being operated at a sampling frequency  $\omega_A$  which is 2 to 1000 times higher than the mixing frequency  $\omega_0$ ;
- a quantization stage, which quantizes at least one of the real part and imaginary part of the control signal which has been up-mixed by  $\omega_0$  and thus produces the pulsed signal;
- a feedback unit, which uses the pulsed signal to produce the feedback signal for the subtraction stage.

48. (CANCELED) The frequency generator as claimed in claim 47, characterized in that the pulse modulator is followed by a bandpass filter, preferably a crystal or ceramic filter.

49. (CANCELED) The frequency generator as claimed in claim 48, characterized in that the pulse modulator has an in-phase signal path for processing of the real part of the input signal, as well as a quadrature signal path for processing of the imaginary part of the input signal.

50. (CANCELED) The frequency generator as claimed in claim 47, characterized in that the control error signal, the control signal and the feedback signal are each complex signals, which each have a real signal component as well as an imaginary signal component.

51. (CANCELED) The frequency generator as claimed in claim 47, characterized in that a noise level is added to the input signal to the quantization stage.

52. (CANCELED) The frequency generator as claimed in claimed 47, characterized in that the feedback unit has a second multiplication stage, which multiplies the pulsed signal by a complex-conjugate mixing signal oscillating at the frequency  $\omega_0$ , and thus produces the feedback signal down-mixed by  $\omega_0$ , for the subtractor.

53. (PREVIOUSLY PRESENTED) A method for pulse modulation of a complex input signal, characterized by the following steps:

- production of a control error signal from the difference between the complex input signal and a feedback signal;
- conversion of the control error signal to a control signal;
- multiplication of the control signal by a complex mixing signal oscillating at the frequency  $\omega_0$ , with at least one of the real part and imaginary part of a control signal, up-mixed by  $\omega_0$ , being produced;
- quantization of at least one of the real part and imaginary part of the control signal, up-mixed by  $\omega_0$ , in order to produce a pulsed signal, with the pulsed signal being used for electrostatic oscillation stimulation of a micromechanical resonator, and with the pulse modulation being carried out at a sampling frequency  $\omega_A$  which is 2 to 1000 times higher than the mixing frequency  $\omega_0$ ;
- production of the feedback signal from the pulsed signal.

54. (PREVIOUSLY PRESENTED) The method as claimed in claim 53, characterized in that the control error signal, the control signal and the feedback signal are each complex signals, which each have a real signal component as well as an imaginary signal component.

55. (PREVIOUSLY PRESENTED) The method as claimed in claim 53, characterized in that the control error signal is converted to the control signal by integrating the control error signal.

56. (PREVIOUSLY PRESENTED) The method as claimed in claim 53, characterized in that the real part of the control signal is multiplied by the real part of the complex mixing signal oscillating at the frequency  $\omega_0$ , and a first result signal is thus produced, and in that the imaginary part of the control signal is multiplied by the imaginary part of the complex mixing signal oscillating at the frequency  $\omega_0$ , and a second result signal is thus produced.

57. (PREVIOUSLY PRESENTED) The method as claimed in claim 56, characterized in that the first result signal and the second result signal are added to form a sum signal in order to determine the real part of the up-mixed control signal.

58. (PREVIOUSLY PRESENTED) The method as claimed in claim 57, characterized in that the sum signal is quantized in order to produce the pulsed signal.

59. (PREVIOUSLY PRESENTED) The method as claimed in claim 53, characterized in that a noise level is added before the quantization of at least one of the real part and imaginary part of the control signal up-mixed by  $\omega_0$ .

60. (PREVIOUSLY PRESENTED) The method as claimed in claim 53, characterized in that the feedback signal is produced by multiplying the pulsed signal by a complex-conjugate mixing signal oscillating at the frequency  $\omega_0$ .

61. (PREVIOUSLY PRESENTED) The method as claimed in claim 53, characterized in that the mixing frequency  $\omega_0$  corresponds to one resonant frequency of the micromechanical resonator.